
Modeling Planetary Motions

Why We Care and How We Do It

Marc A. Murison

Astronomical Applications Department
U.S. Naval Observatory
Washington, DC

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Overview

- ▶ Motivation
- ▶ Context
- ▶ Newcomb
- ▶ Demonstration

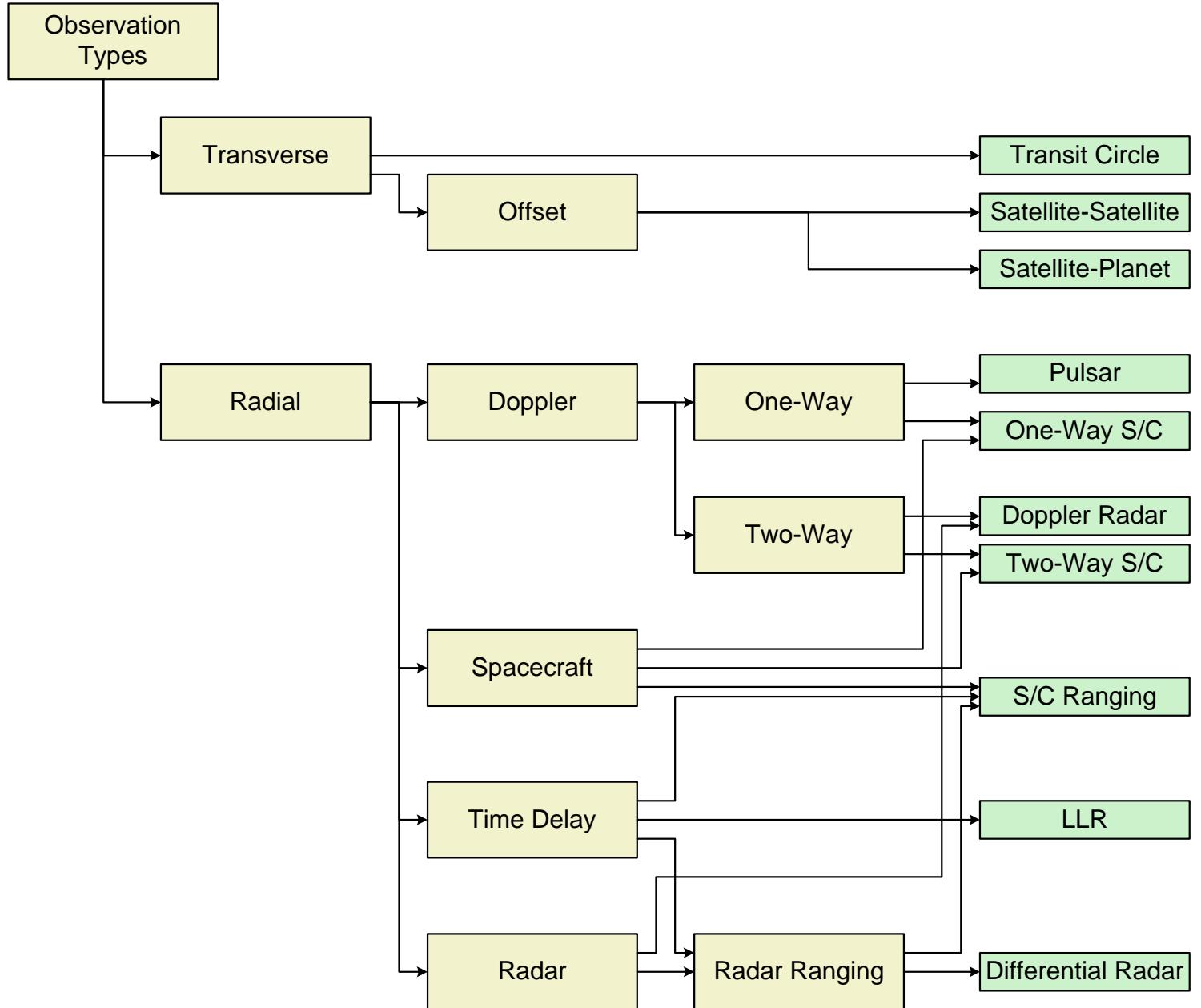
Motivation

- ▶ Why do we need precise **positions**?
 - Navy requirements:
 - stellar positions to 20 milliarcseconds or better
 - stellar reference frame(s) tied to Earth and solar system reference frames
 - Astronomical requirements:
 - Spacecraft navigation
 - Reference frames
 - Weak-field tests of General Relativity
 - Solar system celestial mechanics
 - ▶ Planetary satellites
 - ▶ Trojan satellites
 - ▶ Resonances
 - Asteroid masses
 - ▶ J. Hilton (USNO)
 - Stellar occultations
 - ▶ body geometry
 - ▶ atmosphere probe
 - outer planets
 - Titan

Motivation (continued)

- ▶ Therefore, we need to generate precise **predictions** of planetary positions (ephemerides)
- ▶ Four steps:
 1. Obtain accurate observations
 - optical (ground-based) observations
 - space-based observations (HIPPARCOS, FAME)
 - spacecraft telemetry
 - ground-based radar
 - natural satellite observations
 - planetary positions
 2. Create comprehensive solar system model
 - general relativity
 - Lunar motion
 - Earth rotation
 - planetary topography
 - asteroid masses
 3. Fit model parameters to observations
 4. Create ephemeris

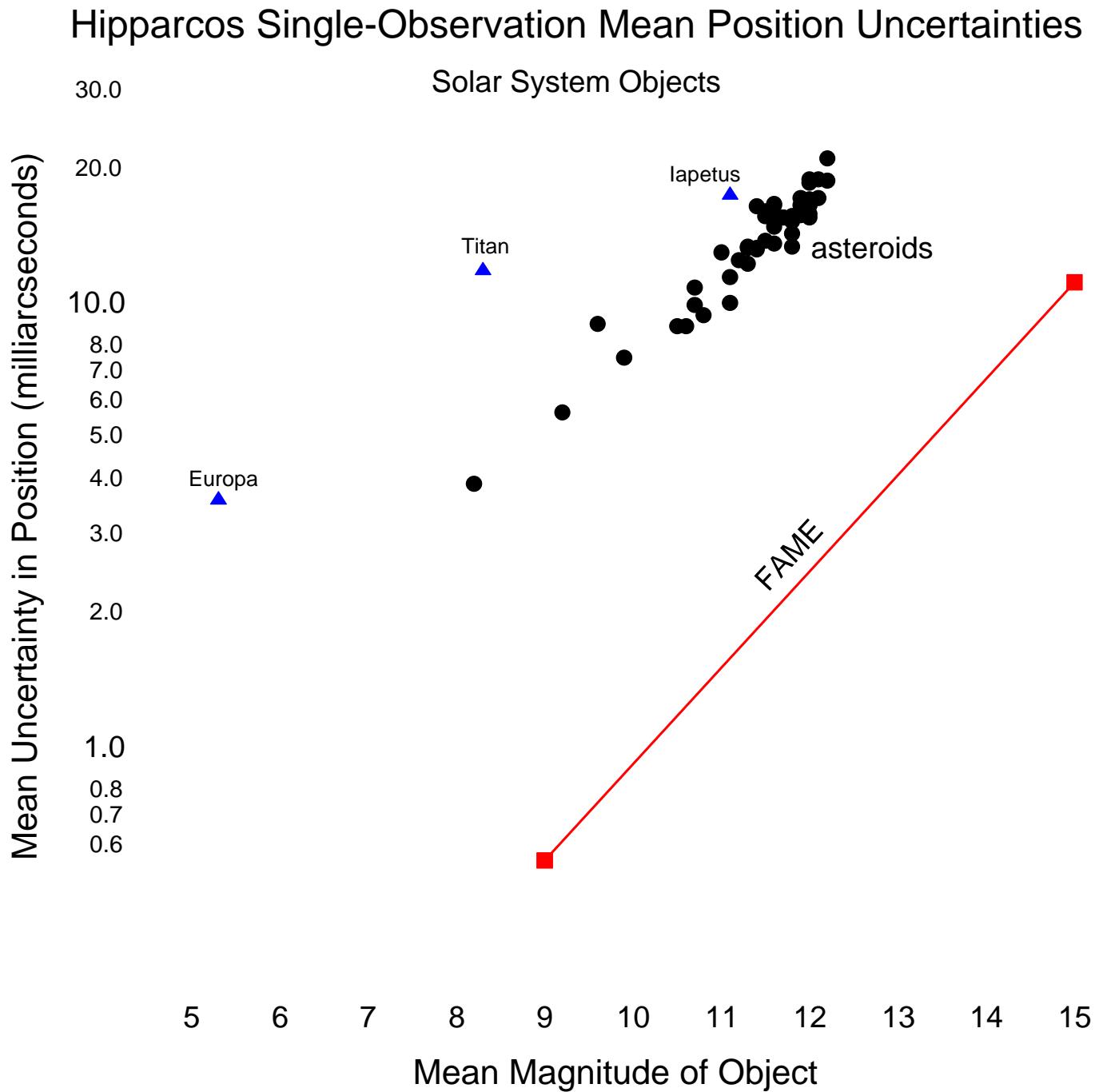
Observation Types



Context

- ▶ Example: space-based natural satellite observations
- ▶ Reference frames
- ▶ Dependencies

Planetary Positions from Satellite Observations



Yikes!

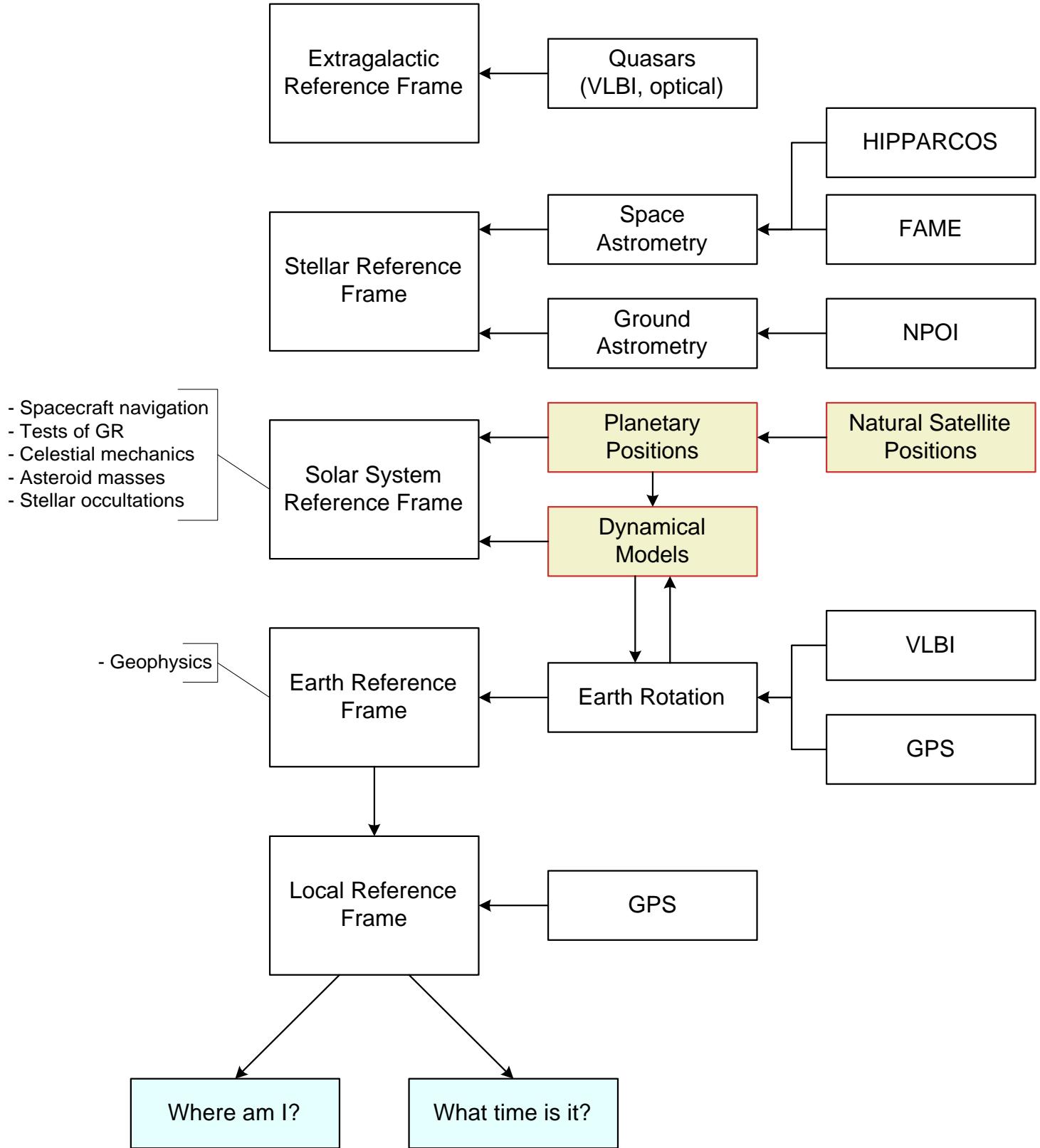
→ How much is a **milliarcsecond**?

- 1 arcsecond \approx 1/16 of an inch around the perimeter of 1000-foot radius Observatory Circle

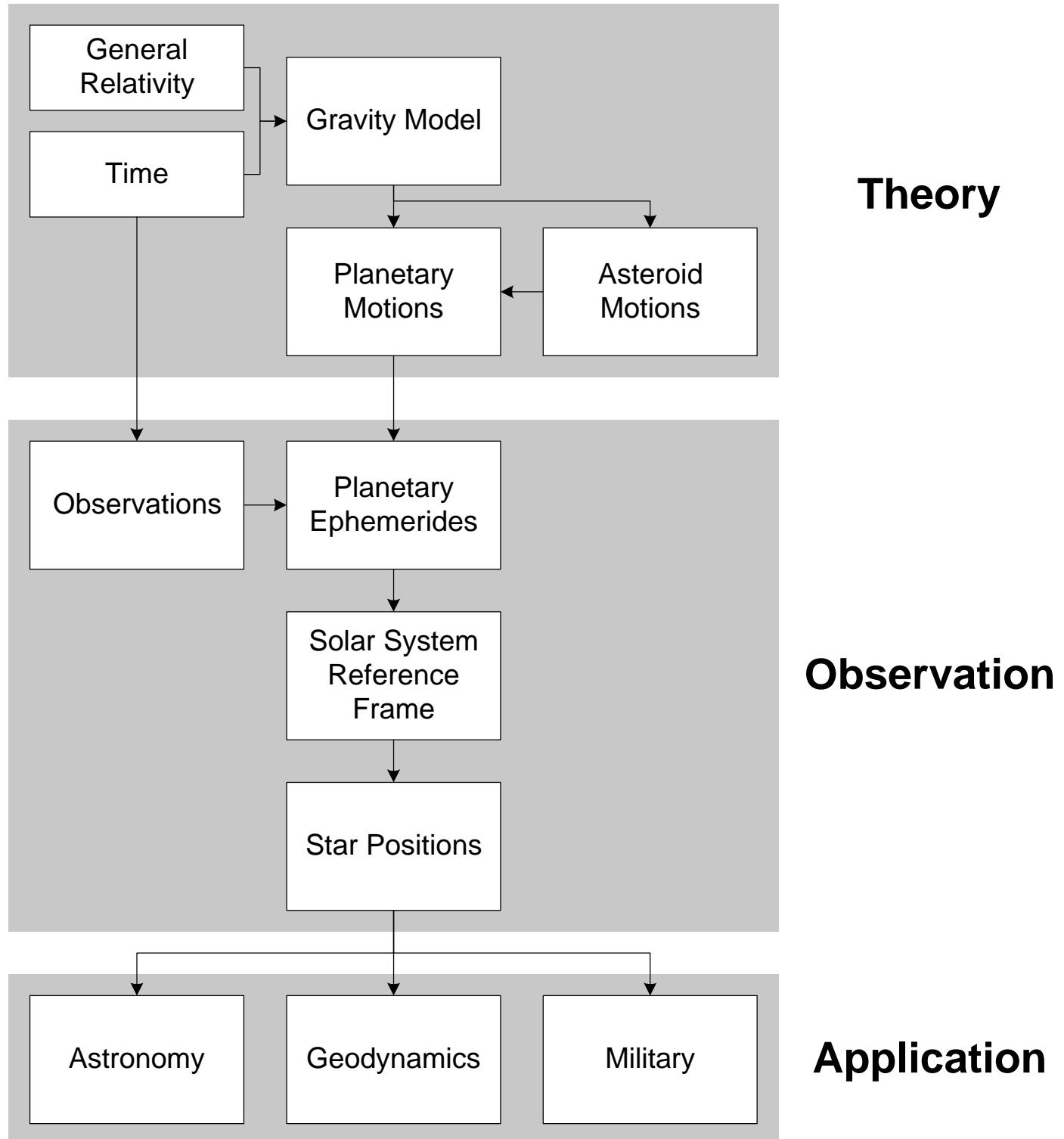
► How much is **50 microarcseconds**?

- the angle subtended by the width of a strand of **human hair** as seen from a distance of **65 miles**

A Hierarchy of Reference Frames



Theory, Observation, and Application



Newcomb: A Solar System Ephemeris Program

- ▶ Motivations
- ▶ Basic process of producing a high-precision ephemeris
- ▶ Demonstration

<http://aa.usno.navy.mil/Newcomb/>

Newcomb: A Solar System Ephemeris Program

► Why a new program?

- Program design and language capabilities are **three generations** beyond the state of the art when DE and PEP were designed.
 - Numerical algorithms
 - Object-Oriented Design (OOD)
 - data encapsulation
 - polymorphism
 - templates
 - Object-Oriented Programming (OOP)
 - fast prototyping
 - safer
 - intuitive
 - We use C++ throughout
 - Graphical User Interfaces (GUIs)
 - Rapid Application Development (RAD) environments
 - "component"-style programming
- Extensibility
 - smaller maintenance burden
 - easily add significant new capabilities

Newcomb: A Solar System Ephemeris Program

- ▶ Why a new program? (cont.)
 - U.S. Naval Observatory
 - capability to generate ephemerides locally
 - ▶ Astronomical Almanac
 - (re)develop in-house expertise
 - ▶ Improvement of planetary theories dates from the very beginnings of the NAO
 - **flexible** research tool for solar system dynamics
 - ▶ dynamical survey of all inner solar system asteroids
 - all mean-motion resonances
 - planetary encounter distributions
 - ▶ investigation of asteroidal noise on Earth, Mars
 - ▶ TNO dynamics
- Independent check of JPL (DE) and CfA (PEP) programs
 - Verify, verify, verify!

PEP Interface

Ephemerides improvement for the first 4 asteroids.

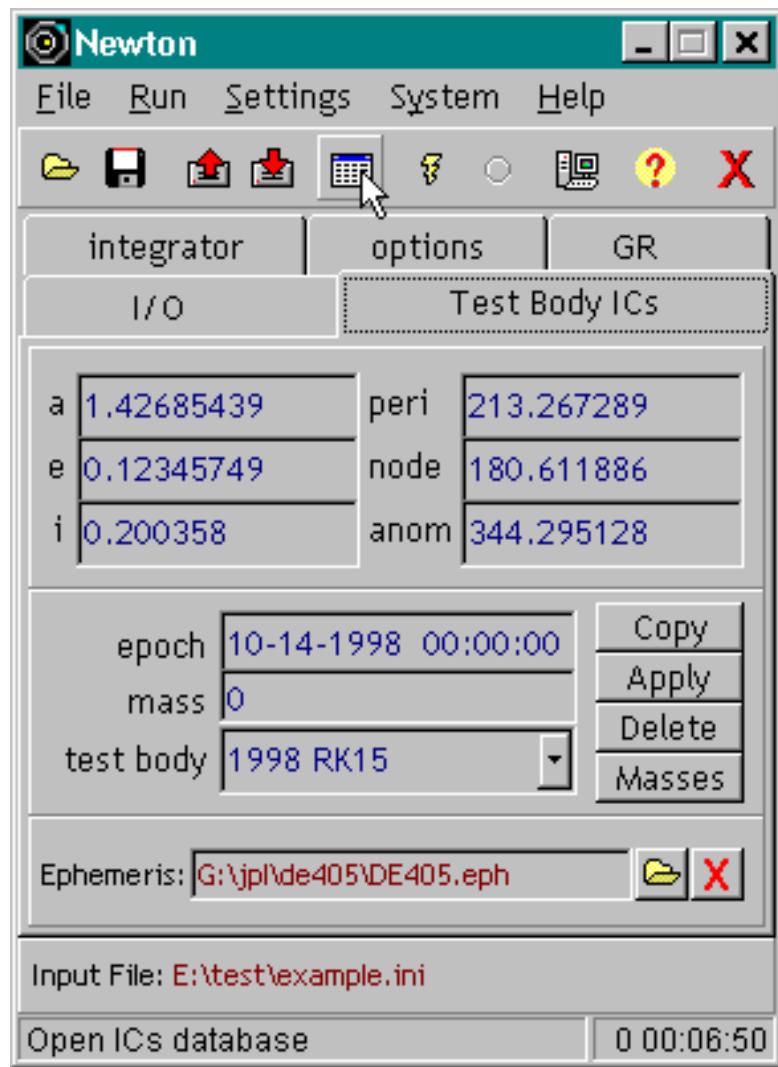
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&NMLST1
EXTPRC= 0,                                $ Use hardware extended precision
ICT(1)= 10,
ICT(3)= 1,                                $ Compute partial derivatives
ICT(4)= 1,                                $ Do not used saved normal equations
ICT(5)= -1,
ICT(9)= 0,
ICT(10)= -2, ICT(11)= -2,
ICT(12)= 2,                                $ prediction or harmonic analysis
ICT(34)= 3,
ICT(39)= 1,
ICT(50)= 1,                                $ USE BROWN MEAN MOON IF NO IPERT
ICT(80)= 0,
JCT(13)= 1,                                $ Use J2000.0 coordinates.
JCT(33)= -1,                               $ Use USNO UT1 and wobble
JCT(27)= 1,                                $ Use * commands
JCT(28)= 7,
MASS(1)= 6023600.D0,                         $ Use DE200 masses for the planets
MASS(2)= 408523.5D0,
MASS(3)= 328900.550000000047D0,
MASS(4)= 3098710.D0,
MASS(5)= 1047.35001090551827D0,
MASS(6)= 3497.99999984177066D0,
MASS(7)= 22960.0000007059389D0,
MASS(8)= 19314.0002382557432D0,
MASS(9)= 130000000.238686755D0,
MASS(10)= 0.012150581D0,
MASS(11)= 2.239D9,
MASS(12)= 9.247D9,
MASS(13)= 8.7D10,
MASS(14)= 7.253D9,
MASS(17)= 1.849D11,
AULTSC= 499.0047837D0,                      $ Length of AU in light seconds
ECINCE= 23.439281083D0,                      $ Use DE118 Obliquity
PRMTER(47)= 0.0D0,                           $ RT. ASC. OF ASCENDING NODE OF ASTEROID BELT
PRMTER(48)= 23.4433D0,                        $ INCLINATION OF ASTEROID BELT
PRMTER(49)= 2.9D0,                            $ DISTANCE OF ASTEROID BELT FROM SUN
PRMTER(50)= 8.773725302941010D-10,          $ MASS OF ASTEROID BELT
PRMTER(81)= 0.0D0,
MDSTSC= 0.,                                 $ MOON TAPE DISTANCE UNIT IN AU
NBODY= 0, IPERT= 10,
NUMOBT= 1,
IOBS = 30,
IOBS1= 14, IOBS2= 15,
$ EPS(3)= 100,
$ EPS(4)= 100,
LPRM(1)= 11, LPRM(2)= 12, LPRM(3)= 14,
*OBJECT EARTH-ROTATION
CON(22)= 5029.0966,
CON(23)= 84381.4119,
*OBJECT 11
NAME= ' CERES ',
INCND= 0, ITAPE= 31, NCENTR= 0, JTYP=6,
A= 2.767121817D0, E= 0.07749262D0, INC= 27.116375D0,
ASC= 23.471566D0, PER= 133.40890D0, ANOM= 2.08129D0,
JD1= 2378801, JD2= 2450001, JDO= 2444801,
K(31)= 1, K(32)= 1, K(33)= 1, K(34)= 1, K(35)= 1, K(36)= 1, K(37)= 1,
K(38)= 1, K(39)= 1, K(40)= 1, K(41)= 1, K(42)= 1, K(43)= 1, K(44)= 1,
K(61)= 1,                                $ Include General Relativity
K(87)= 2, INT= 2,                          $ INTERVALS
K(88)= 2, K(89)= 6,                        $ ADAMS-MOULTON METHOD, 7 TERMS
K(91)= -3, K(92)= -6, EPS(3)= 1E-9 $ STARTING INTERVALS
K(98)= -500, K(99)= 0, K(100)= -1, $ PRINT + TAPE; ORDINARY EQNS OF MOTION
KI= 1, 1, 1, 1, 1, 1, 12, 13, 14,
L= 1, 1, 1, 1, 1, 1,
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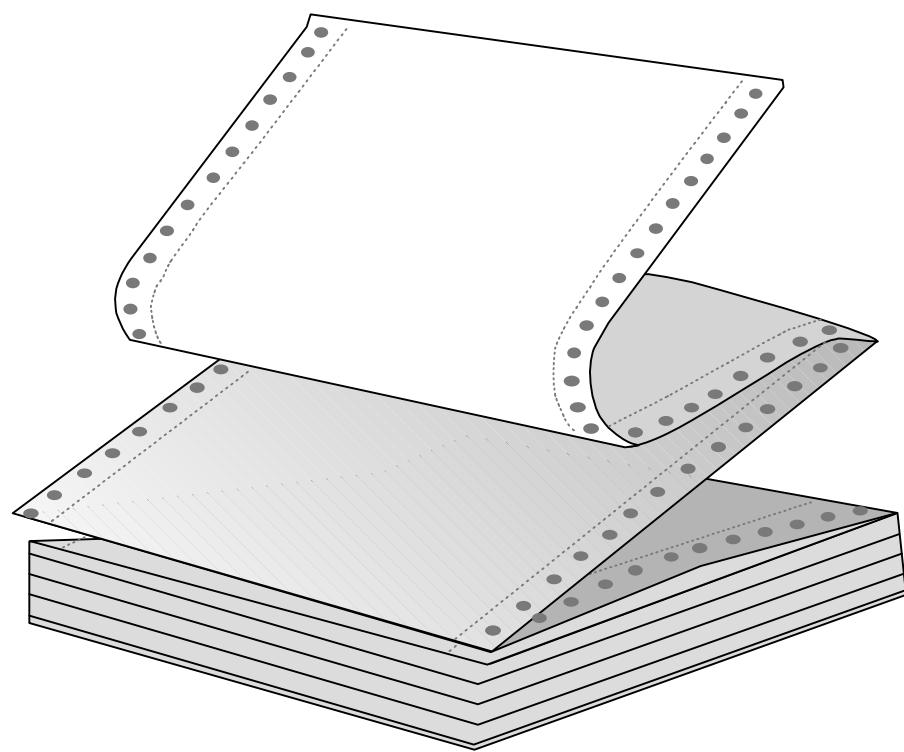
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K(31)= 1, K(32)= 1, K(33)= 1, K(34)= 1, K(35)= 1, K(36)= 1, K(37)= 1,
K(38)= 1, K(39)= 1, K(40)= 1, K(41)= 1, K(42)= 1, K(43)= 1, K(44)= 1,
K(61)= -1,
K(87)= 4, INT= 4,                          $ INTERVALS
K(88)= 2, K(89)= 6,                        $ Adams-Moulton integrator, 7 terms
K(91)= -3, K(92)= -6, EPS(3)= 1E-9, $ Starting intervals
K(98)= -500, K(99)= 0, K(100)= -1, $ Print & tape, ordinary eqns. of motion
KI= 1, 1, 1, 1, 1, 1, 1, 1,
L= 1, 1, 1, 1, 1, 1, 1, 1,
*OBJECT 14
NAME= ' VESTA ',
INCND= 0, ITAPE= 34, NCENTR= 0, JTYP= 6,
A= 2.362114063D0, E= 0.08961581D0, INC= 22.717580D0,
ASC= 18.187358D0, PER= 237.48420D0, ANOM= 308.51911D0,
JD1= 2381051, JD2= 2450001, JDO= 2444801,
K(31)= 1, K(32)= 1, K(33)= 1, K(34)= 1, K(35)= 1, K(36)= 1, K(37)= 1,
K(38)= 1, K(39)= 1, K(40)= 1, K(41)= 1, K(42)= 1, K(43)= 1, K(44)= 1,
K(61)= 1,                                $ Include General Relativity
K(87)= 2, INT= 2,                          $ INTERVALS
K(88)= 2, K(89)= 6,                        $ ADAMS-MOULTON METHOD, 7 TERMS
K(91)= -3, K(92)= -6, EPS(3)= 1E-9 $ STARTING INTERVALS
K(98)= -500, K(99)= 0, K(100)= -1, $ PRINT + TAPE; ORDINARY EQNS OF MOTION
KI= 1, 1, 1, 1, 1, 1, 1, 11,
L= 1, 1, 1, 1, 1, 1, 1, 1,
*OBJECT 27
NAME= ' Arete ',
INCND= 0, ITAPE= 37, NCENTR= 0, JTYP= 6,
A= 2.73942088D0, E= 0.1630220D0, INC= 26.08786D0,
ASC= 20.12111D0, PER= 310.03548D0, ANOM= 168.77030D0,
JD1= 2407351, JD2= 2450002, JDO= 2450001,
K(31)= 1, K(32)= 1, K(33)= 1, K(34)= 1, K(35)= 1, K(36)= 1, K(37)= 1,
K(38)= 1, K(39)= 1, K(40)= 1, K(41)= 1, K(42)= 1, K(43)= 1, K(44)= 1,
K(61)= 1,                                $ Include General Relativity
K(87)= 2, INT= 2,                          $ INTERVALS
K(88)= 2, K(89)= 6,                        $ ADAMS-MOULTON METHOD, 7 TERMS
K(91)= -3, K(92)= -6, EPS(3)= 1E-9 $ STARTING INTERVALS
K(98)= -500, K(99)= 0, K(100)= -1, $ PRINT + TAPE; ORDINARY EQNS OF MOTION
KI= 1, 1, 1, 1, 1, 1, 1, 14,
L= 1, 1, 1, 1, 1, 1, 1, 1,
*SITES
WASHUSNO 6378.14014 77.067451477 38.921340942 0 0 0-3
LEONUSNO 6380.438 69.33167 -31.80278 0 0 0-3
LaPalma 6380.468 17.8817 28.7600 0 0 0-3
GRENEWICH 6378.189 0.00000 51.47728 0 0 0 0
Bordeaux 6378.213 0.5283 44.835 0 0 0-3
6378.213 .00335364
CAPETOWN 6378.153 -18.47864 -33.93519 0 0 0 0
EDINBURG 6378.274 3.18425 55.92500 0 0 0 0
CAMBRIDG 6378.169 -0.09479 52.21433 0 0 0 0
SEEB 6378.463 -10.71045 50.94386 0 0 0 0
MILAN 6378.260 -9.19117 45.46647 0 0 0 0
PALERMO 6378.216 -13.35779 38.11222 0 0 0 0
OTTAWA 6378.225 75.8933 45.3869 0 0 0 0
PARIS 6378.207 -2.337619 48.8364 0 0 0 0
TOULOUSE 6378.334 -1.4625 43.61222 0 0 0 0
NICE 6378.478 -7.30208 43.72136 0 0 0 0
BESANCON 6378.452 -5.98833 47.24936 0 0 0 0
UCCLE 6378.245 -4.1358114 50.79844 0 0 0 0
G TOKYO 6378.199 -139.540750 35.67261 0 0 0 0
*EECORR
PALE SCHU 1 0 1 0.1824 0.0000 1.954
MILA SCHU 1 0 1 0.0638 0.0000 -1.914
GREN SCHU 1 0 1 0.0000 0.0000 0.0000
GREN 1530 1 0 1 0.2628 0.0000 -3.158
GREN 3679 1 0 1 0.0595 0.0000 -0.040
GREN 8096 1 0 1 0.0727 0.0000 -0.352
CAMB SCHU 1 0 1 0.0950 0.0000 -0.406
CAMB COLD 1 0 1 0.1496 0.0000 0.757
EDIN SCHU 1 0 1 0.1794 0.0000 0.186
PARI SCHU 1 0 1 0.0033 0.0000 0.982
PARI 6479 1 0 1 0.0450 0.0000 0.149
SEEB SCHU 1 0 0 -0.0509 0.0000 0.0000
GREN G189 1 0 1 0.0268 0.0000 -0.118
WASH WA25 1 0 1 -0.0051 0.0000 0.027
WASH W350 1 0 1 -0.0377 0.0000 -0.017
WASH W450 1 0 1 -0.0493 0.0000 -0.049
WASH W550 1 0 1 -0.0587 0.0000 -0.056
LEON WL50 1 0 1 -0.0582 0.0000 0.028
WASH W650 1 0 1 -0.0103 0.0000 -0.116
LaPa L890 1 0 1 -0.0056 0.0000 -0.051
$Bord BV85 1 0 1 0.0000 0.0000 0.0000
**END
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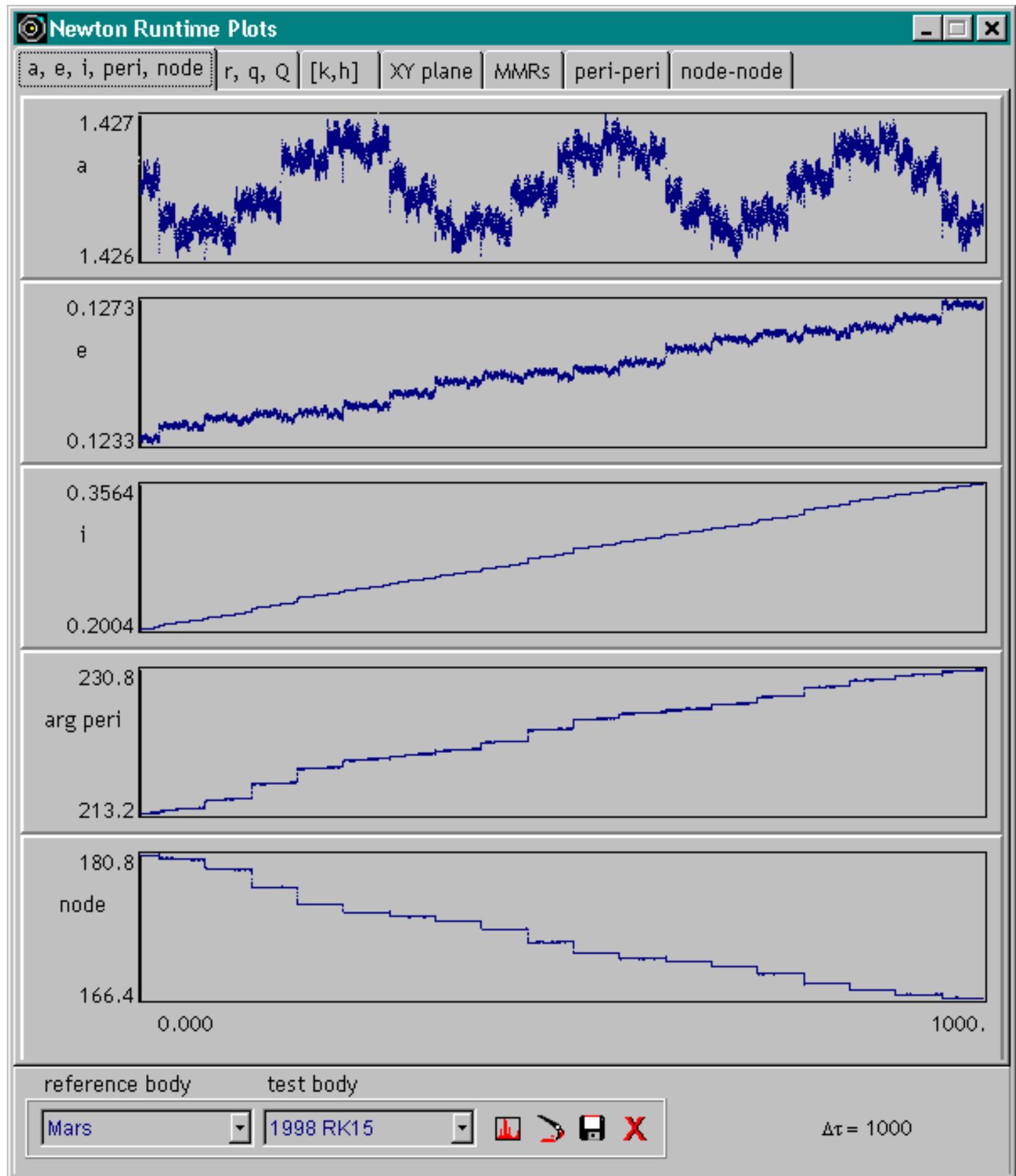
Newcomb Interface



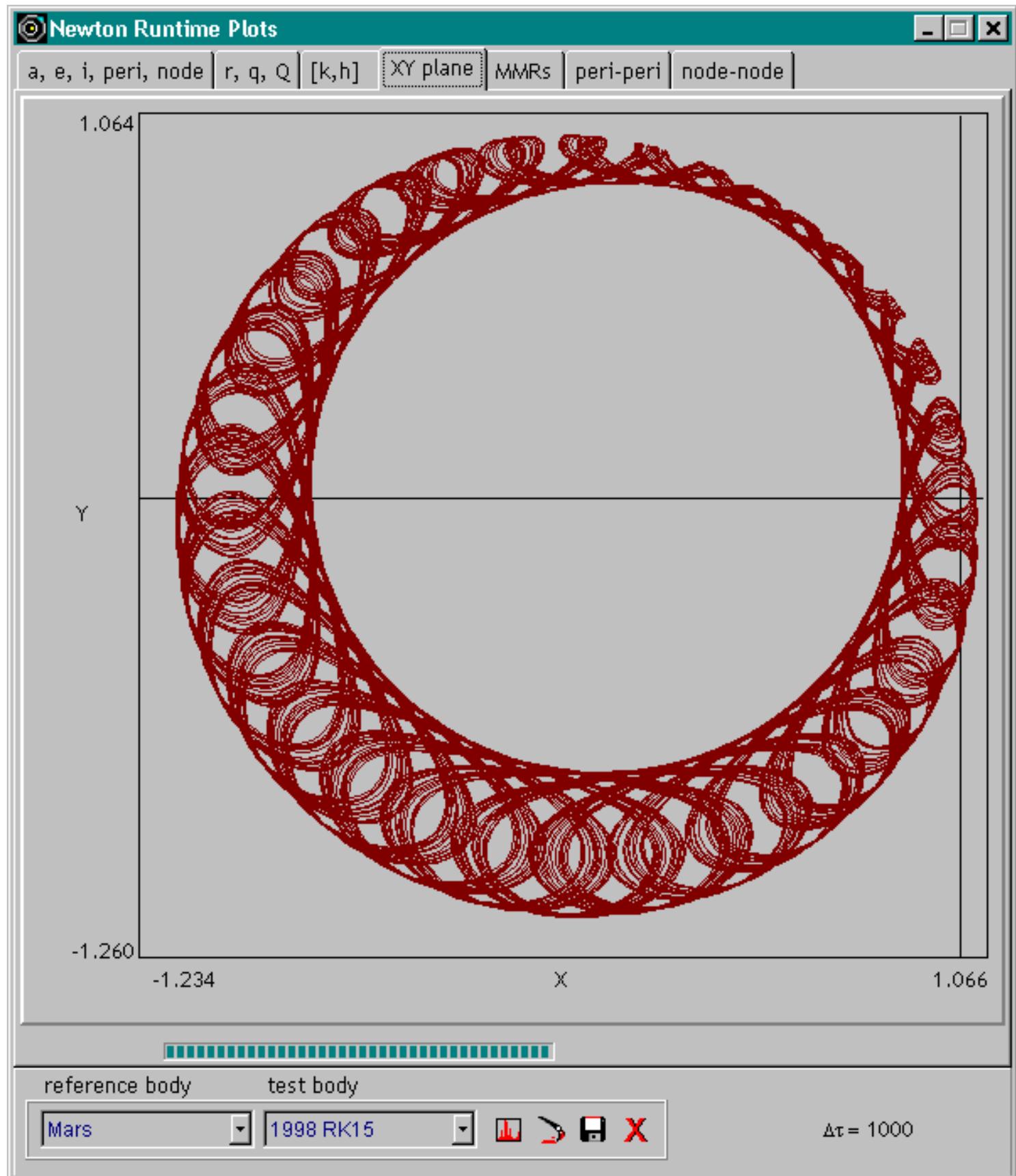
PEP Quick-Look



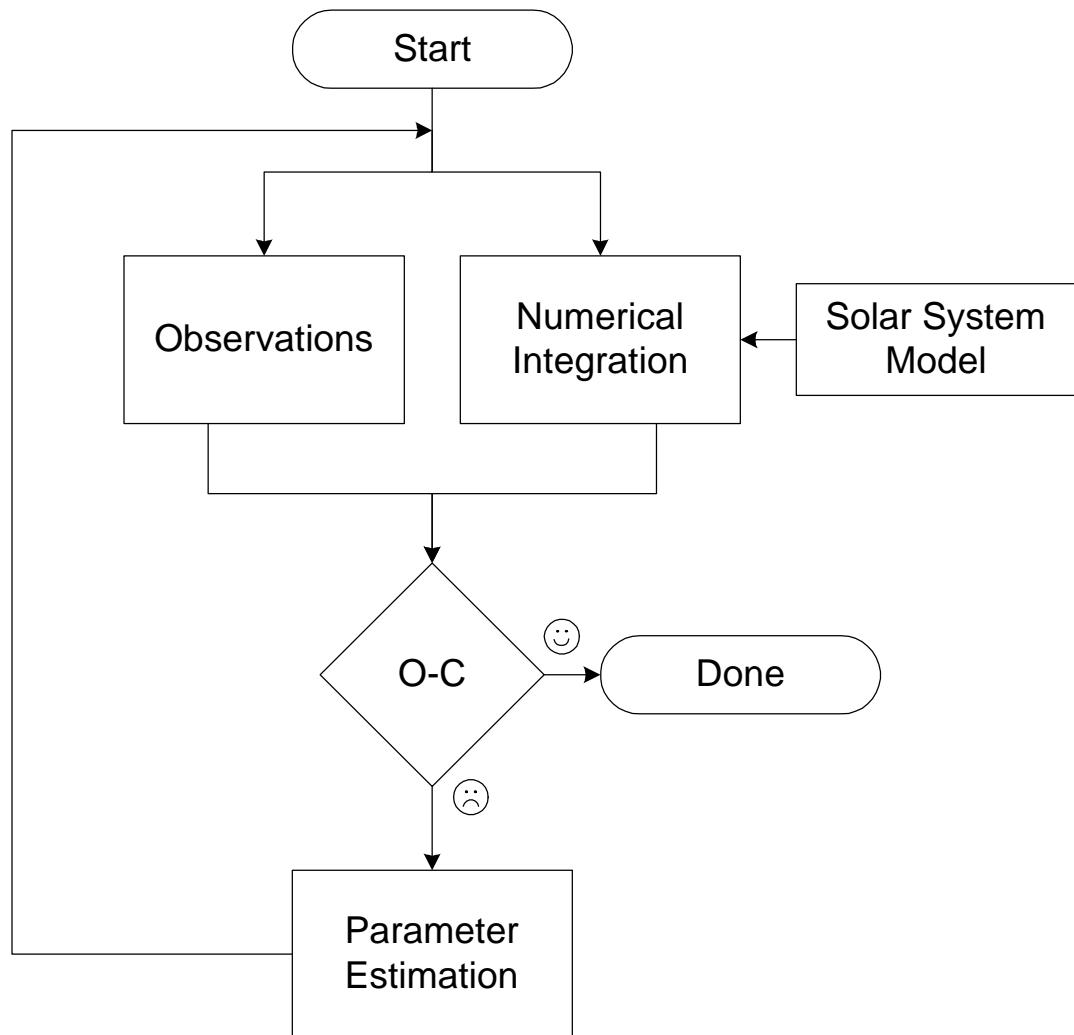
Newcomb Quick-Look



Newcomb Quick-Look



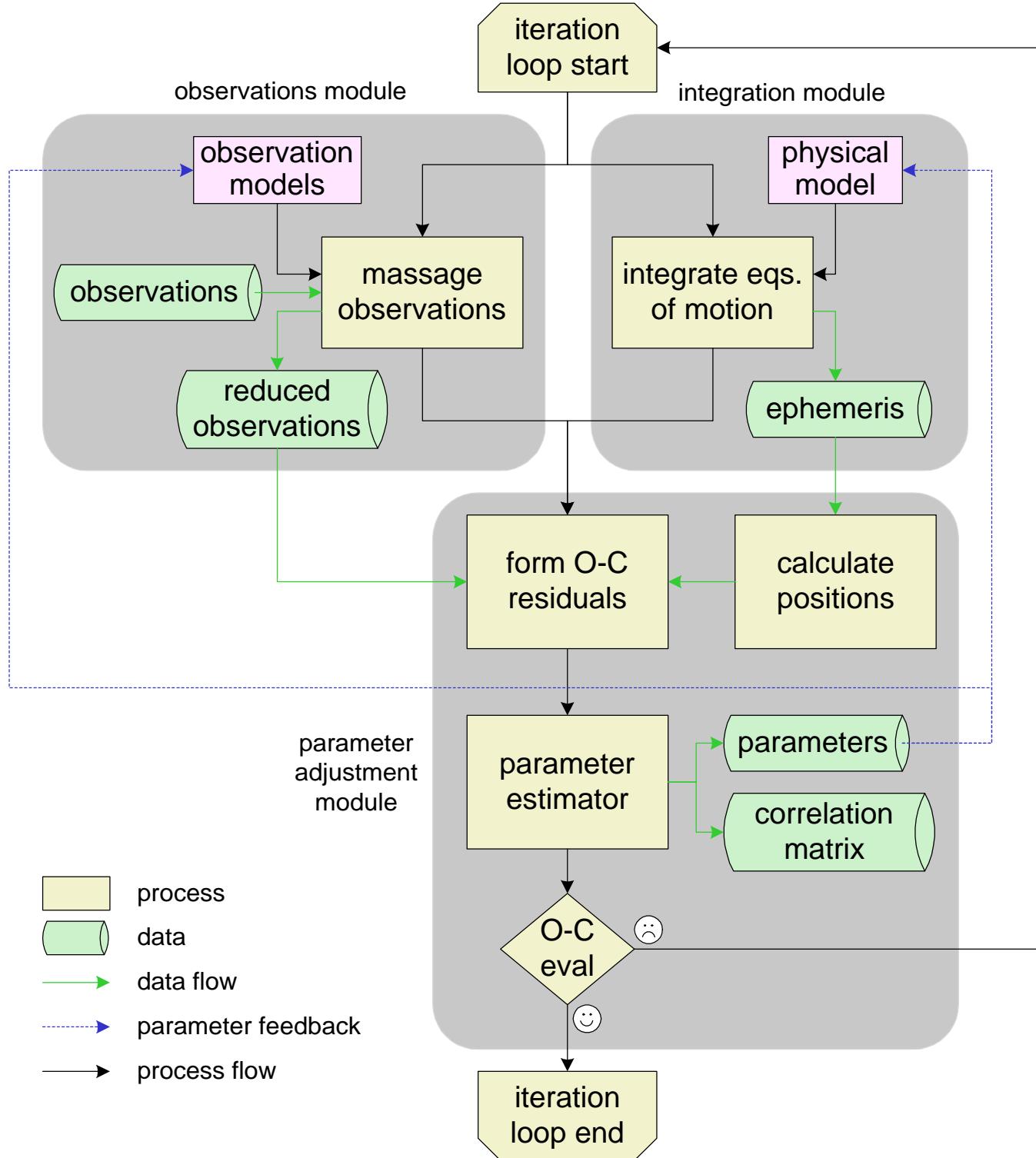
Newcomb Outline



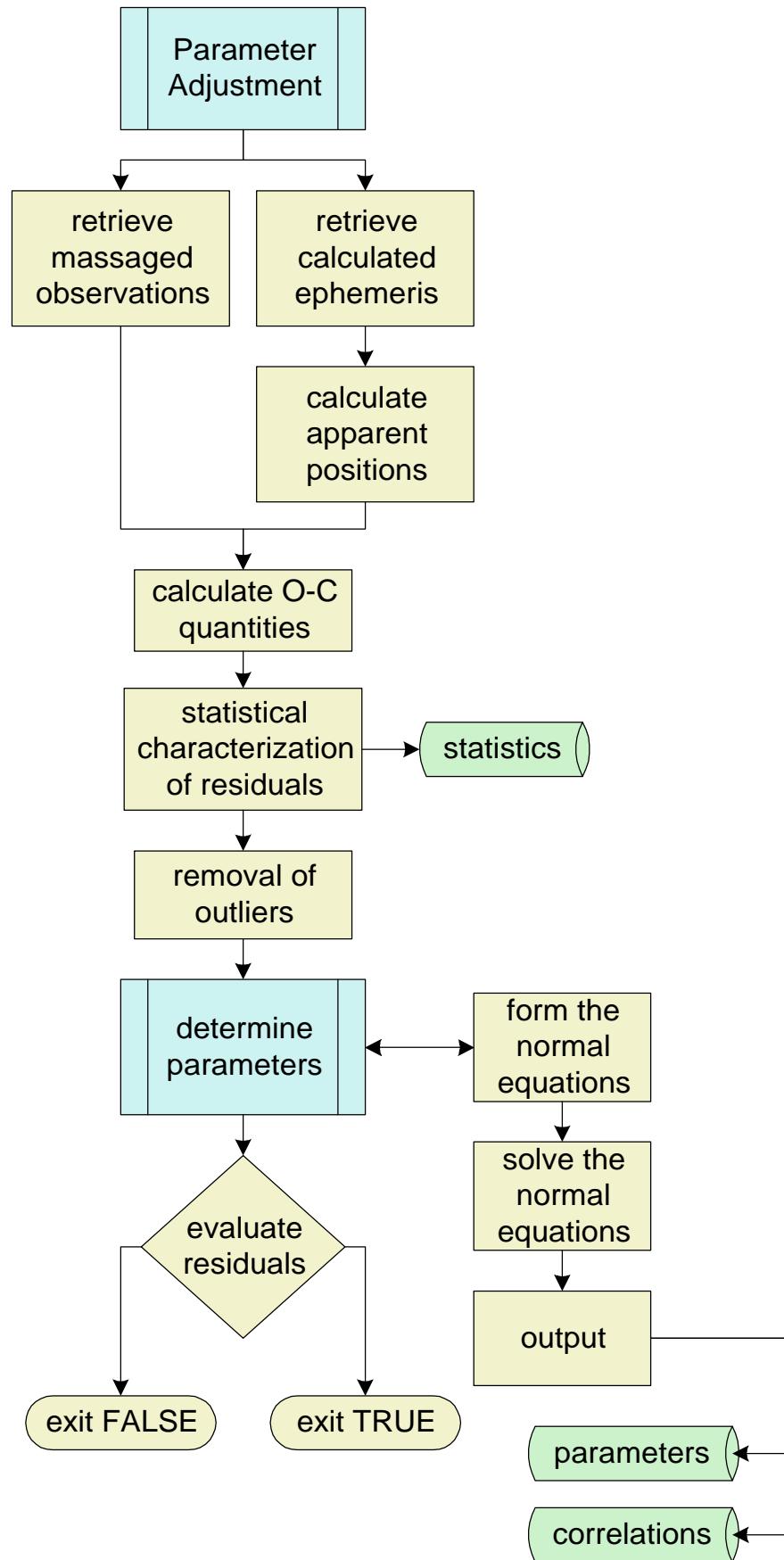
(An Aside)

- ▶ Eckert and the first digital machine: ~1 ms to multiply two 10-digit numbers
 - Factor of $\sim 10^8$ improvement
- ▶ This machine (266 MHz PII): 11 ns to multiply two 15-digit numbers
 - Factor of $\sim 10^5\text{-}10^6$ improvement

Process Outline (Detailed)



Parameter Adjustment Module



Integration Module

